

Kinetics of Divalent Metals (Cd^{2+} , Cu^{2+} , Pb^{2+} , Zn^{2+}) Adsorption onto a Modified Brick

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Authors' contributions

This work was carried out in collaboration between all authors. This experimental work was performed by author OA as part of his thesis. Authors MW and AB supervised the work.

Author AB collected experimental data and wrote the manuscript. Author JM was at the origin of this research project and helped to gain financial supports as government principal private secretary (State Minister) in Central African Republic. All authors read and approved the final manuscript.

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ABSTRACT

Brick which originated from Bangui Region (in Central African Republic), was pre-activated with HCl at 90°C and coated with ferrihydrite. This material was used in the present work as an adsorbent mainly for the removal of metallic cations ($\text{Me}^{2+} = \text{Cd}^{2+}$; Cu^{2+} ; Pb^{2+} ; Zn^{2+}) from aqueous solutions due to their bad effect on the environment. Experimental results were compared to those obtained for other divalent cations (Ca^{2+} , Fe^{2+} , Mg^{2+} , Mn^{2+} , Sr^{2+}). Freundlich and Langmuir models were applied to describe adsorptions isotherms, and Langmuir model was found to provide the best fitting. Langmuir adsorption capacities (Q_{max}) of these ions onto ferrihydrite-coated brick increased in the following order: $\text{Cu} > \text{Zn} > \text{Pb} > \text{Ca} > \text{Cd} > \text{Mg}$. Kinetic studies revealed that experimental data were better fitted by the pseudo second-order rate equation than the pseudo first-order rate one. Thermodynamic analyses indicated that the adsorption kinetics process was endothermic. Because of acid/hydrolysis characteristics of metallic

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cations, the kinetic constant, k_2 , was found to be affected by H^+ and OH^- (i.e., solution pH) as potential-determining ions by regulating proportions of negative and positive charges at the brick surface. The adsorption capacity (Q_e) was determined from kinetic data and the adsorption affinity of the studied eight elements onto $\equiv S-OH$ sites in modified brick had the following order: $Pb > Cu > Cd \approx Mn \approx Zn > Mg > Ca > Sr$. These Q_e values were found to be instead related to the surface binding constant, $K_{(\equiv S-O)Me}$, relative to the equilibrium: $(\equiv S-OH) + Me^{2+} \leftrightarrow (\equiv S-O)Me^+ + H^+$, suggesting the implication of hydroxyl groups from brick metakaolinite in addition to $-OH$ and/or $-ONa$ functions mainly present in ferrihydrite deposits.

Keywords: Brick; ferrihydrite; metakaolinite; divalent cation; adsorption; isotherm; kinetics; complexation.

1. INTRODUCTION

Aqueous metal ions are known to be toxic, even at very low concentrations, and their presence in wastewaters, ground waters for instance, the maximum acceptable concentration of Cd^{++} , Cu^{++} , Zn^{++} and Pb^{++} recommended by the World Health Organization (WHO) for drinking water is : $3\mu g/L$, $10\mu g/L$, $3\mu g/L$ and $2\mu g/L$, respectively . High levels of these metals pose risks to human health, mainly : *Cadmium*, because of its carcinogenic, mutagenic and teratogenic effects, and as endocrine disruptor and it causes chronic anemia and renal failure; *Copper*, it causes brain and kidney damages, chronic anemia, liver cirrhosis, and stomach/intestinal irritations; *Zinc*, it can cause dizziness and fatigue; and *Lead*, because of its harmful effects on the development, intelligence and memory of children, and it is also known to increase the risks of renal failure and cardiovascular disease [1]. This explains why the removal of metal ions from aqueous solutions is nowadays considered as one of the great problems on water treatments worldwide. To remove heavy metals from contaminated waters, numerous purification-treatment technologies have been developed over the last decades [2-8]. Among them, adsorption has gained importance for this task, and some natural materials (such as: chitosan, fly ash, coal, zeolite, clays, agricultural waste materials) have been used successfully as low-cost adsorbents [9-12]. To enhance the sorption of these natural adsorbents towards heavy metals, chemical modifications of their surfaces with metal oxide(s) /hydroxide(s) have often been made [13]. For instance, the impregnation of zeolite with iron (or manganese) oxides resulted in high removal efficiency of copper(II) and lead(II) from aqueous solutions [14-16].

On this view, we have recently proposed brick as a low cost, no toxicity, easily available, effective and reusable adsorbents for the removal of metal cations from aqueous environment [17-21]. Thus, water treatments based on using modified brick is now tested in rural areas of Central African Republic where this material (which is commonly made by local craftsmen) can be obtained by African population in large quantities and cheap. This brick is mainly composed of sand and metakaolinite, and to a lesser extent, of iron oxides [17]. Moreover, iron oxide / hydroxide used alone as a separate phase is commonly referred as an adsorbent to remove metal cations from wastewaters. However, its direct use in a separation / filtration system is very difficult mainly because of its fine particle size. But the coating with a thin layer of iron hydroxide (as ferrihydrite) onto HCl-activated brick pellets has proved to enhance significantly adsorption capacity for divalent metals when compared to raw brick [20-21]. It is well known that the complexity of naturally occurring ferrihydrite is due to the presence of inorganic impurities including: silicon and aluminum that can affect its

composition, crystallinity, solubility and even its thermodynamic stability. Micro-analyses permitted us to detect the presence of Al and Si in brick ferrihydrite (Allahdin et al. unpublished works), suggesting structural incorporation to surface complexation and/or surface precipitation as, e.g.: strong-binding ligands from brick clays being suspected to be associated with the surface of ferrihydrite particles.

In this work, modified brick was used as a cations adsorbent in deionized water and the common metallic pollutants Cd^{++} , Cu^{++} , Zn^{++} and Pb^{++} were selected as adsorbates because of their bad effect on aquatic media. Adsorption properties of other cations were also examined in the present work only for data comparison: Ca^{2+} , Fe^{2+} , Mg^{2+} , Mn^{2+} , Sr^{2+} . It should be noted that: (i) the adsorption process was examined here only in single-metal system (and not in multi-metals system); and (ii) data on desorption isotherms and desorption rate were not reported here (although numerous works are under way in our lab in the role of added inert electrolytes on the kinetic rate, the importance of bleach in the regeneration process of brick, and the implication of electrostatic forces induced by H^+ and/or OH^- ions as potential determining ions on the adsorption capacity of brick). Langmuir and Freundlich isotherms were used to assess the equilibrium data. The adsorption kinetics was studied at varying temperatures based on the pseudo-first and pseudo-second-order kinetics models. The implication of acidic (hydrolysis) properties of divalent cations in water on the adsorption process was studied.

2. MATERIALS AND METHODS

2.1 Adsorbent Preparation and General Characteristics

The raw brick used in this study was obtained from Bangui region in the Central African Republic. Previously, X-ray diffraction and chemical analysis were performed on this material: ~ 61 wt % quartz; ~ 21 wt % metakaolinite; 3-4 wt % illite; ≤ 4 wt % iron oxides / hydroxides; and ≤ 2 wt % feldspar + mica + biotite [17]. Before use, several physical / chemical treatments were carried out on the raw brick [17,18]. Briefly: (i) it was broken into grains and sieved with sizes ranging from 0.7 to 1.0 mm; (ii) the resulting particles were leached with a 6M HCl solution at 90°C for 3 hours; and (iii) finally a deposition of FeOOH onto HCl - treated brick was made by precipitation of iron(III) with a NaOH solution up to attain pH ~ 7. After these chemical treatments, resulting particles were sized again with 0.7-1.0 sizes, and some of their physical characteristics were assessed: surface area, 70 m²/g; pore volume, 0.21 cm³/g; and density 0.845 ± 0.027 g/dm³.

Chemical and spectroscopic analyses were previously performed on brick samples [18, 21]. Briefly, it was found that: (i) after acid leaching of raw brick at 90°C, Al content decreased in the porous material and FT-IR spectroscopy permitted us to detect Brönsted (protonic) and Lewis (aprotonic) acid sites at the surfaces of grains [18]; and (ii) after FeOOH deposition ²³Na MAS NMR revealed the involvement of sorbed Na⁺ ions to form outer-sphere complexes with the active brick sites, and ¹H MAS NMR further showed only a broad line shape which was caused by dipole-dipole interactions between brick protons (when water molecules diffused on the brick surface and visited the various types of hydroxyl groups: Si-OH, Al-OH, and Fe-OH) [21]. It is worth noting that the interaction of Me²⁺ ions with brick led to a chemical combination "Me²⁺--brick" with several 1H MAS NMR resonances which were ascribed to protons of silanols and aluminols in the brick [21].

2.2 Chemicals

All chemicals used in the study were analytical grades. Sodium hydroxide and hydrochloric acid were supplied by DISLAB (France). The following salts: $\text{Cd}(\text{NO}_3)_2 \cdot 4\text{H}_2\text{O}$, $\text{Fe}(\text{NO}_3)_3 \cdot \text{H}_2\text{O}$, and $\text{Pb}(\text{NO}_3)_2$ were purchased from Prolabo. $\text{Cu}(\text{NO}_3)_2 \cdot 3\text{H}_2\text{O}$ was obtained from Scharlau, $\text{Ca}(\text{NO}_3)_2 \cdot 4\text{H}_2\text{O}$, $\text{Mg}(\text{NO}_3)_2 \cdot 6\text{H}_2\text{O}$, $\text{Sr}(\text{NO}_3)_2$, $\text{FeCl}_2 \cdot 4\text{H}_2\text{O}$ and $\text{Mn}(\text{NO}_3)_2 \cdot 4\text{H}_2\text{O}$ were purchased from Merck, and $\text{Zn}(\text{NO}_3)_2 \cdot 6\text{H}_2\text{O}$ from Fluka. For kinetics experiments, divalent - metal salts were first diluted in Milli-Q water to obtain a 7.16×10^{-3} mole-per-liter solution (in the case of iron, this concentration corresponded to 400 mg per liter); The stock solutions of cationic metals were second diluted ten-fold to obtain an experimental-solution concentration of 7.16×10^{-4} mol-per-liter.

2.3 Isotherm Studies

To study the adsorption behavior of the metal ions on modified brick, the experiments for adsorption isotherms were performed at room temperature and under constant stirring condition. Isotherm studies on divalent cations (Ca^{2+} , Cd^{2+} , Cu^{2+} , Mg^{2+} , Pb^{2+} and Zn^{2+}) adsorption onto Bangui brick were carried out on brick grains with 0.7 -1.0 mm sizes. These experiments were performed in ten 100mL-flasks –each one containing 1g of brick pellets— in which were added 50 mL of a divalent-cation solution with a concentration ranging from 1.15×10^{-4} to 7.80×10^{-4} mol/L. These flasks were placed on a mechanical (orbital) shaker (Model: IKA Labortechnik KS 250 basic) and gently shaken at a speed of 120 rpm. Adsorption-isotherm experiments lasted one night although a reaction time of 4 hours at a temperature of $17^\circ\text{C} \pm 1^\circ\text{C}$ was sufficient for the system to attain thermodynamic equilibrium. Afterwards, suspensions were filtered and the recovered solution was analyzed to determine cation concentrations using an ICP-AES (Inductively Coupled Plasma Atomic Emission Spectroscopy; Model: Varian Pro axial view) spectrometer. The quantity of solute adsorbed onto brick pellets, noted Q_e (in mg/g), was assessed from the difference between the initial and the equilibrium contents of cationic ions in the liquid phase. It should be noted that all these experiments were at least triplicated and data were averaged.

2.4 Kinetic Studies

For each kinetic experiment, 1 g of modified brick pellets (with average diameters varying from 0.7 to 1.0 mm) was added to 100 mL of the diluted metal solution (7.16×10^{-4} mol/L) at a fixed temperature. This suspension was continuously and gingerly mixed with a propeller stirring and pH was measured during the process. 1 mL of the supernatant (which was filtered through a $0.45 \mu\text{m}$ pore diameter cellulose nitrate filter) was collected at various time intervals from 0 to 60 minutes and analyzed for the determination of metal level by ICP-AES. The reproducibility of concentration measurements was ensured by repeating three times the same experiments under identical experiment conditions. This procedure permitted us to determine average values of metal content in the reaction solution, and standard deviations of these analyses were evaluated to be within $\pm 3\%$. The $\text{Me}(\text{II})$ adsorption capacity of brick was calculated by using the following equation: $Q_e = (\text{Co} - \text{Ce})V/m$, where Q_e represents the adsorption capacity of divalent metal on FeOOH -coated brick (in mg/g); Co is the initial content of Me^{2+} ions in the cell (in mg/L); Ce represents the equilibrium solute concentration (in mg/L); and m and V correspond to the mass of brick used (g) and the volume of $\text{Me}(\text{II})$ solution used (L), respectively. At this metal concentration (7.16×10^{-4} mol/L), Fe^{2+} ions remained at oxidation state II under our physicochemical (O_2 , natural potential E_h and pH) conditions, according $p_e - \text{pH}$ diagrams for iron-water system [22].

3. RESULTS AND DISCUSSION

3.1 Adsorption Isotherms

In order to relate the adsorbate concentration in the bulk solution with the adsorbed content present at the adsorbent surface, several adsorption equations were proposed in the literature [23-33]. Two of them were selected for this work: Langmuir and Freundlich ones [23,25,33]. The Langmuir –isotherm model was *first* applied to our systems by assuming that the observed adsorption occurred onto homogeneous brick surfaces with a specific number of equivalent sites. For fitting of the experimental data, a linear form of Langmuir model was used [25,33]:

$$\frac{1}{Q_e} = \frac{1}{Q_{\max}} + \frac{1}{bQ_{\max}C_e} \quad (1)$$

where C_e is the concentration of metal ions at equilibrium in the solution (mg/L); Q_e represents the amount of divalent metals adsorbed at brick surfaces (mg/g); Q_{\max} corresponds to the amount of metal ions at complete monolayer coverage (mg/g), and b is Langmuir constant which depends upon the adsorption energy. The parameters, b and Q_{\max} , were calculated from the intercepts and slopes of the Langmuir plots of $1/Q_e$ against $1/C_e$ that were drawn for the different studied cations (see Fig. 1 and Table 1).

The Freundlich-isotherm model was *second* applied to our systems by assuming, in this case, the existence of several types of adsorption sites on heterogeneous brick surfaces. This model could be described by the following equation [23,33]:

$$\text{Log}Q_e = \text{Log}K_F + \left(\frac{1}{n}\right)\text{Log}C_e \quad (2)$$

Where K_F is the sorption capacity constant (mg/g); and n is the sorption intensity constant K_F and n were calculated from the intercepts and slopes of the Freundlich plots of $\text{Log}Q_e$ against $\text{Log}C_e$ (see Fig. 1 and Table 1).

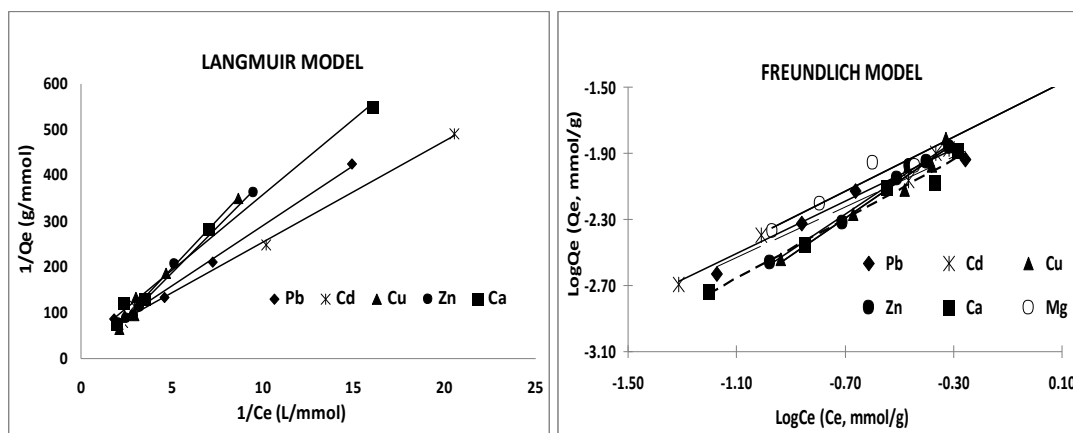


Fig. 1. Adsorption isotherms of some divalent cations on modified brick fitted using Langmuir and Freundlich models at room temperature.

Table 1. Langmuir and Freundlich constants for the adsorption of some divalent cations by modified brick in water at room temperature.

	Q_{max} $\mu\text{mol/g}$	b L/mg	K_F mg/g	n	R_L
Cu^{2+}	100.5	0.0029	0.1781	0.8994	0.86-0.94
Zn^{2+}	79.5	0.0063	0.1879	0.9158	0.83-0.95
Pb^{2+}	37.0	0.0050	0.3198	1.3098	0.55-0.89
Ca^{2+}	27.1	0.0286	0.2229	1.1173	0.60-0.92
Cd^{2+}	24.0	0.0815	0.5521	1.6804	0.41-0.85
Mg^{2+}	22.1	0.0935	0.2707	1.2143	0.45-0.75

Overall, our findings revealed that our experimental data fitted Langmuir isotherm better than Freundlich one, with a regression coefficient $R^2 > 0.997$. Therefore, this adsorption process acted more as a monolayer adsorption on the surface of modified brick under our applied experimental conditions. The maximum adsorption capacity, Q_{max} , from the Langmuir isotherm was found to decrease in the following order: $\text{Cu(II)} > \text{Zn(II)} > \text{Pb(II)} > \text{Ca(II)} > \text{Cd(II)} > \text{Mg(II)}$. Comparable adsorption-capacity values were previously found for iron(II): 12-28.6 $\mu\text{mol/g}$ [18,19]. Variable physico-chemical phenomena were involved in these systems because of different hydrolysis characteristics of these cations, and thereby these complicated any interpretation of this order.

To further predict whether or not the study adsorption was favorable, a dimensionless separation factor — which was associated with the Langmuir isotherm and called equilibrium parameter (R_L)— was calculated from the following equation [34]:

$$R_L = \frac{1}{1 + bC_0} \quad (3)$$

where C_0 represents the initial concentration of divalent cations in the medium (in mg/L). The value of R_L permitted us to show whether the adsorption process was: irreversible ($R_L = 0$); favorable ($R_L < 1$); linear ($R_L = 1$); or unfavorable ($R_L > 1$) [34]. Indeed, the fact that all the R_L values obtained in this work for the adsorption of cationic entities on modified brick were in the range of 0.41 – 0.95 (see Table 1), implied that this adsorption process was favorable. In addition, the n values for the different cations were found to be higher than 1, indicating a (moderately) favorable adsorption mechanism. A comparison of the maximum capacities of these cations on ferrihydrite - coated (pre-activated) brick with those on other iron-bearing minerals —which were reported as promising metals adsorbents in the literature— was made in the present work (see Table 2). It should however be noted that because of variation in parameters and experimental conditions applied, direct comparison with other published data ought to be considered as tentative. It could nevertheless be noticed that the material used in this work possessed adsorption characteristics somewhat close enough to those observed for different iron-bearing adsorbents cited in the literature (see Table 2). Moreover, in our investigations the Q_{max} values were found to be strongly dependent upon the content of ferrihydrite coating the brick surface. This, when calculating the adsorption capacity by referring directly to the amount of ferrihydrite deposited onto brick pellets, Q_{max} could theoretically reach values up to 100 times higher than those obtained in this work. This implied that, if pre-activated brick was sufficiently impregnated with ferrihydrite, the resulting material should possess an additional potential for practical application in heavy-metal removals from wastewaters.

Table 2. Comparison of adsorption performance of ferrihydrite-coated brick for divalent-cations removals with those observed for other iron oxide-bearing materials

Coating	Support material	Adsorbed divalent metals	Removal performance mmol/g	Refs.
Ironoxide	Alumina	Pb	Pb (0.14)	[35]
	Bentonite	Pb	Pb (0.107)	[36]
	Sand	Cu ; Pb	Cu (0.004) ; Pb(0.006)	[37]
	Sand (ferruginous)	Cu	Cu (0.032)	[38]
	Sewage sludge	Cu ; Cd ; Pb	Cu (0.27); Cd (0.13); Pb (0.21)	[39]
	Waste silica gel	Cu ; Cd ; Pb	Cu (0.053); Cd (0.038); Pb (0.039)	[40]
	Sepiolite	Pb	Pb (0.366)	[41]
Goethite	Sand	Cd; Pb	Cd (0.006); Pb (<0.001)	[42]
	Sand (quartz)	Cd	Cd (0.002)	[43]
	Clinoptilolite	Cu; Pb	Cu (0.004); Pb (0.006)	[44]
		Cu; Zn	Cu (0.5); Zn (0.2)	[45]
Hydrated ferric oxide	Polyacrylamide	Cd; Pb	Cd (1.309); Pb (1.020)	[46]
Fe, Mg hydr(oxides)	Bentonite	Pb	Pb (0.463)	[47]
Ferrihydrite	(Pre-activated) brick (*)	Fe(II) in Bangui ground waters (§)	Fe (0.015)	[20]
	(Pre-activated) brick (*)	Ca; Cd; Cu; Mg; Pb; Zn	Ca (0.037); Cd (0.024); Cu (0.100); Mg (0.022); Pb (0.037); Zn (0.079)	This work

(*) Raw brick made in Bangui region (Central African Republic) was first pre-activated with a 6M-HCl solution at 90°C for 3 hours (and, second impregnated with ferrihydrite by Fe(III) precipitation with NaOH to pH 7).

(§) Modified brick was tested in soluble iron(II) removals from Bangui ground waters.

3.2 Adsorption Kinetics

Adsorption-kinetics studies were useful in assessing the metal - ions uptake rate and in gaining information about the study mechanism [47]. To investigate the kinetics of the heterogeneous reaction between cationic entity and brick, it was preliminarily important to monitor how fast the reaction took place under our experimental conditions.

Concentration removal of metal ions from solution at different temperatures and under constant stirring condition was determined by ICP-AES. For instance, Fig. 2 shows how the concentration of Pb(II) varied with time during several experiments performed at temperatures ranging from 20 - 35°C.

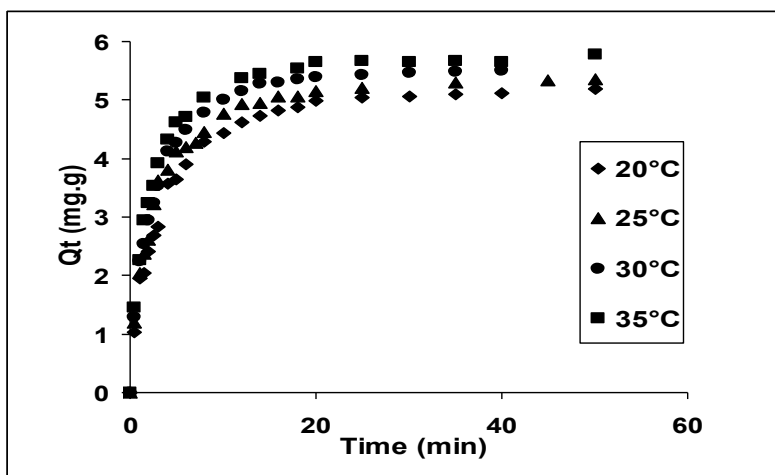


Fig. 2. Effect of temperature on the adsorption kinetics of Pb²⁺ ions by modified brick grains.

Brick = 4g, [Cation] = 7.16 × 10⁻⁴ mol/L, Volume = 100 mL.

Overall, it was found that: (i) the adsorption process was quite rapid in the first 20 min and about 1 hour was necessary to reach an equilibrium state (Fig. 2); and (ii) an increase in the temperature resulted in increasing Pb(II) adsorption rate (Fig. 2), thus revealing the process to be endothermic. This will be confirmed and detailed in section 3.3. Similar trends were found for the removal of the other cations studied here (*i.e.*, Cd²⁺, Cu²⁺, Mg²⁺, Sr²⁺, and Zn²⁺) from water by modified brick in a similar temperature range. Two kinetics models—namely pseudo-first-order and pseudo-second-order—were used in this work. For these kinetics studies, we had taken in account James and Healy's suggestions [10], *i.e.*: adsorption cannot depend upon the appearance of a specific ionic species such as the first or other hydrolysis product and even specific polynuclear complexes. In this assumption, the pseudo-first-order kinetic rate expression (Lagergren equation) could be given as [48, 49]:

$$\ln(Q_e - Q_t) = \ln(Q_e) - k_1 t \quad (4)$$

where Q_e and Q_t (mg/g) represent the amounts of divalent cation (Cd²⁺, Cu²⁺, Mg²⁺, Pb²⁺, Sr²⁺ and Zn²⁺) adsorbed per unit weight of brick at equilibrium and time t (min), respectively; and k_1 (1/min) is the rate constant of pseudo-first-order sorption. The pseudo-second-order kinetics rate expression (Ho equation) could be given as [48,50]:

$$\frac{t}{Q_t} = \frac{1}{k_2 Q_e^2} + \frac{t}{Q_e} \quad (5)$$

Where k_2 (g/(mg.min)) is the rate constant of pseudo-second-order adsorption. The plots of $\ln(Q_e - Q_t)$ versus t and t/Q_t versus t gave straight lines (see Fig. 3). The values of k_1 , k_2 , and Q_e were obtained from the intercepts and slopes of these straight lines.

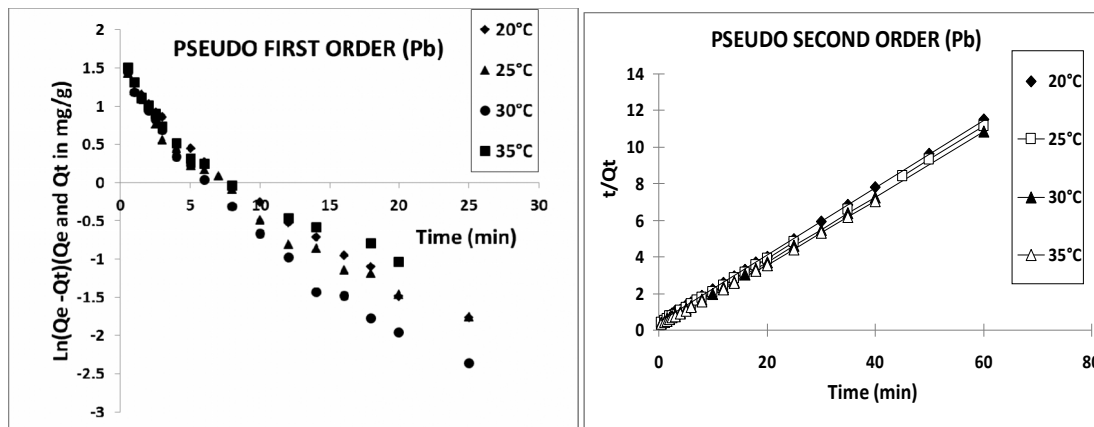


Fig. 3. Pseudo-first order and pseudo-second order kinetic plots, $\ln(Q_e - Q_t)$ vs t and t/Q_t vs t , for the adsorption of divalent cations onto modified brick grains at 298°K.

Q_e and Q_t (mg/g) are the amounts of adsorbed cations at equilibrium and time t (min), respectively.

Kinetics parameters calculated from linear plots of both models and correlation coefficient values are given in Table 3. It was noticed that the adsorption kinetics data fitted both models very well ($R^2 > 0.9$). However, good linearity of the Lagergren pseudo-first-order plot observed for these divalent cations was no assurance that the process would follow first-order kinetics. Indeed, adsorption data were found to fit better the pseudo-second-order model judging by higher R^2 values ($R^2 > 0.998$; see Table 3). Furthermore, as reported in Table 3 experimental and theoretical Q_e values of the second-order model revealed better consistencies, when compared to the first-order model. Therefore, these findings implied that the adsorption process adhered more to the pseudo-second-order kinetics. Such a model then assumed that one divalent cation (Me^{2+}) was adsorbed onto two sorption sites (noted 2A) on the brick surface according to [19]:

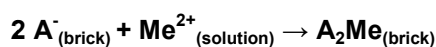


Table 3. Pseudo-first-order and pseudo-second-order kinetics parameters measured at different temperatures for the adsorption of some divalent cations onto modified brick in Milli-Q water. pH_i is the 'initial' pH value measured at the beginning of the reaction

	T°K	pH_i	Pseudo-first order kinetics				Pseudo-second order kinetics			
			$Q_e \text{ exp.}$ ($\mu\text{mol/g}$)	$Q_e \text{ cal.}$ ($\mu\text{mol/g}$)	k_1 (1/min)	R^2	$Q_e \text{ cal.}$ ($\mu\text{mol/g}$)	k_2 (g/(mg.min))	k_2 (g/(mM. min))	R^2
Pb^{2+}	293	5.3	25.17	12.71	0.097	0.9507	26.1	0.085	17.637	0.9998
Cu^{2+}	294.2	5.51	21.72	16.43	0.19	0.9624	22.53	0.361	22.947	0.9992
Cd^{2+}	293.2	6.9	20.88	14.02	0.204	0.9926	21.46	0.255	28.608	0.9996
Zn^{2+}	295.1	6.49	17.27	10.26	0.16	0.9549	17.4	0.529	34.593	0.9993
Mg^{2+}	293.2	8.09	14.59	7.37	0.172	0.9437	14.97	2.073	50.379	0.9996
Sr^{2+}	294.8	8.69	9.91	9.5	0.3	0.9841	10.38	0.645	56.489	0.9976
Pb^{2+}	298	5.31	25.95	11.39	0.099	0.9532	26.65	0.107	22.233	0.9998
Cu^{2+}	298.2	5.47	24.07	15.65	0.136	0.9776	25.3	0.255	16.204	0.9993
Cd^{2+}	298.2	6.87	19.76	11.09	0.2	0.9612	20.14	0.286	32.111	0.9997
Zn^{2+}	298.5	6.5	16.3	12.86	0.174	0.9966	16.94	0.689	45.066	0.9993
Mg^{2+}	298.2	7.94	14.33	8.49	0.239	0.9084	14.84	2.211	53.743	0.9985

Table 3 Continue.....

Sr ²⁺	300	8.58	10.7	7.22	0.262	0.9683	11.05	0.833	73.023	0.9989
Pb ²⁺	303	5.67	26.68	12.23	0.127	0.9483	27.41	0.119	24.719	0.9997
Cu ²⁺	303.2	5.42	22.23	15.76	0.218	0.9349	22.55	0.5	31.741	0.9991
Cd ²⁺	303.2	6.81	21.23	12.65	0.171	0.9694	21.26	0.319	35.904	0.9994
Zn ²⁺	303.3	6.53	16.81	11.99	0.197	0.9754	17.27	0.731	47.767	0.9996
Mg ²⁺	303.2	7.92	13.78	5.67	0.113	0.9052	13.71	3.006	73.056	0.999
Sr ²⁺	303.2	8.55	9.56	9.98	0.332	0.9891	11.25	0.759	66.539	0.9981
Pb ²⁺	308	5.71	27.33	15.86	0.122	0.9341	28.63	0.131	27.102	0.999
Cu ²⁺	308.2	5.39	21.52	11.33	0.11	0.8997	20.96	0.438	27.808	0.9974
Cd ²⁺	308.2	6.78	21.53	11.75	0.201	0.9669	22.11	0.356	39.996	0.9997
Zn ²⁺	308.2	6.57	18.21	8.74	0.205	0.959	18.64	0.826	53.997	0.9997
Mg ²⁺	308.2	7.87	13.67	11.01	0.688	0.8798	13.67	3.442	83.648	0.9996
Sr ²⁺	308.3	8.47	9.85	9.64	0.381	0.9992	10.15	1.001	87.734	0.9987

3.3 Adsorption Activation Energy Kinetics

In the above section, the pseudo second-order model was identified as the best kinetic model for mathematical treatment of our experimental data. In the present section the rate constant, k_2 , of the pseudo-second order model was used to evaluate the activation energy of the adsorption process by using Arrhenius equation:

$$\ln(k_2) = \ln(A) - \frac{E_a}{RT} \quad (6)$$

where A and E_a are the Arrhenius factor and the activation energy, respectively; and R and T are the ideal gas constant (8.314J/(mol.K)) and the absolute temperature ($^{\circ}$ K), respectively. By plotting $\ln(k_2)$ versus $1/T$ (for instance for Pb(II); see Fig. 4) and from the slopes and intercepts, E_a values for the different divalent-cations adsorption reactions could be attained. The positive values of E_a suggested that increase in temperature favored the adsorption process. Consequently, the study mechanism was an endothermic one in nature. To know whether the adsorption process was mainly physical or chemical one, it was previously suggested that activation energies should range from ~ 5 to ~ 40 kJ/mol for physisorption reactions and from ~ 40 to ~ 800 kJ/mol for chemisorption ones [51-53]. All the E_a values obtained in this study were found to be < 40 kJ/mol (see Table 4), indicating that studied Me^{2+} -ions adsorption reactions possessed low potential barriers and were dominantly assigned to a physisorption phenomenon [51,52,54].

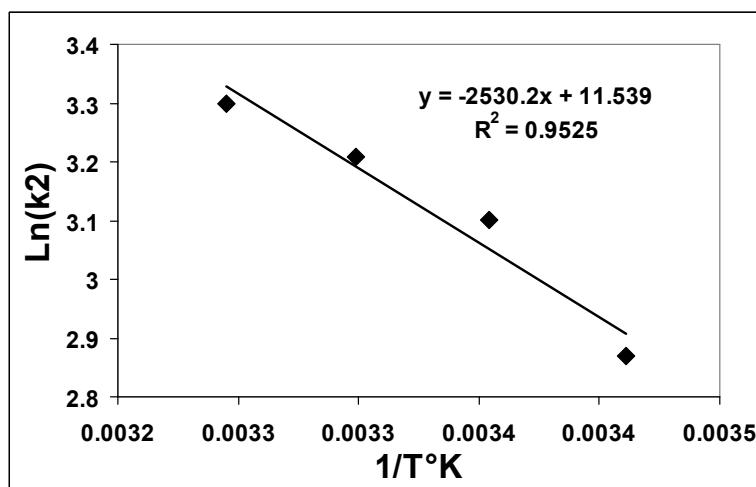


Fig. 4. Arrhenius plot, $\text{Ln}(k_2)$ vs $1/T$, for the adsorption of Pb^{2+} ions on modified brick grains at 298°K . k_2 is expressed in $\text{g}/(\text{mM}\cdot\text{min})$.

Physisorption needs little energy to perform, whereas chemisorption demands much higher energies. Moreover, brick was negatively charged at the medium pH and thereby should attract positive ions at its surface [55]. Therefore, owing to the implications of electrostatic forces, physisorption should be predominant in this adsorption process, as pointed out by Li and his coworkers [55]. To know whether the adsorption process involved activated (intermediate) complexes, the enthalpy (ΔH_a) and the entropy (ΔS_a) of activation were assessed using Eyring equation:

$$\text{Ln} \left(\frac{k_2}{T} \right) = \text{Ln} \left(\frac{k_B}{h} \right) - \frac{\Delta H_a}{RT} + \frac{\Delta S_a}{R} \quad (7)$$

Table 4. Thermodynamic parameters for the adsorption kinetics of divalent cations onto modified brick

Ea	Thermodynamic parameters of pseudo-second order kinetics						
	ΔH_a	ΔS_a	ΔG_a (293°K)	ΔG_a (298°K)	ΔG_a (303°K)	ΔG_a (308°K)	
<i>kJ/mol</i>	<i>kJ/mol</i>	<i>J(mol.K)</i>	<i>kJ/mol</i>	<i>kJ/mol</i>	<i>kJ/mol</i>	<i>kJ/mol</i>	
<i>Pb</i>	20.997	18.510	-178.40	70.781	71.673	72.565	73.457
<i>Cu</i>	20.919	18.416	-168.53	67.795	68.638	69.480	70.323
<i>Cd</i>	16.769	14.271	-184.11	68.214	69.135	70.056	70.976
<i>Zn</i>	23.281	20.768	-155.83	66.426	67.205	67.984	68.763
<i>Mg</i>	27.588	25.108	-153.46	70.072	70.839	71.606	72.373
<i>Sr</i>	21.522	19.017	-160.45	66.029	66.831	67.633	68.436

Where k_B is Boltzmann constant; h is Planck constant; and the other parameters are already defined above. The plots of $\text{Ln}(k_2/T)$ versus $1/T$ were found to be straight lines (for instance for Pb: see Fig. 5), and their slopes and intercepts were used to calculate ΔH_a and ΔS_a (see Table 4). Furthermore, the Gibbs free energy of activation, ΔG_a , could be expressed in terms of enthalpy and entropy of activation as follows:

$$\Delta G_a = \Delta H_a - T\Delta S_a \quad (8)$$

The ΔG_a values obtained for the different adsorption reactions between divalent cations and brick grains varied from ca +60 to +71 kJ/mol at 298°K (see Table 4). Note that the free energy of activation can be obtained from the rate constant, (k) through the Activated Complex Theory equation (also known as Eyring-Polanyi equation): $k = C \exp(-\Delta G_a/RT)$, where C is a constant. And like this work, positive ΔG_a values were found either for metal adsorptions [56] or geochemical transformations [57].

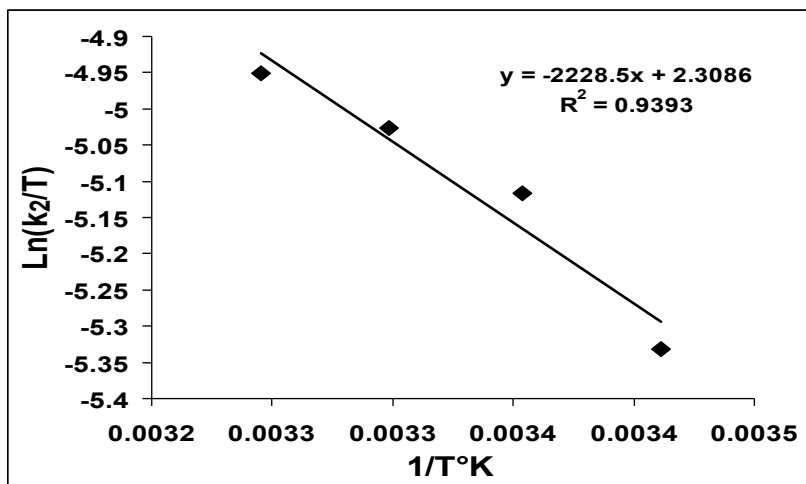


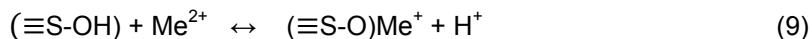
Fig. 5. Eyring plot, $\text{Ln}(k_2/T)$ vs $1/T$, for the adsorption of Pb^{2+} ions on modified brick grains at 298°K.

k_2 is expressed in the International System.

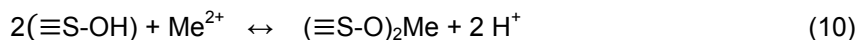
The positive values of ΔH_a (ranging from ca. +14 to +21 kJ/mol; see Table 4) showed that this process consumed energy and thereby was endothermic. As for activation entropy, their negative values (ranging from ca. -153 to -178 J/(mol.K); see Table 4) suggested two features: (i) partial orders occurred at the beginning of the kinetic step due to electrostatic attraction phenomena [55], before any structural (chemical) changes at the adsorbent /ferrihydrite surface; and (ii) schematically metal ion was adsorbed onto brick surface through the formation of an activated (intermediate) complex according to an associative mechanism [58,59,60]. It is worth noting that these thermodynamic (activation) parameters revealing the relevance in the energetics of the kinetic heterogeneous process studied, are in the range of those reported in the literature concerning kinetics of metal adsorption on adsorbents like activated carbon [56] and even of various geochemical transformations [57].

3.4 Interpretation of the Adsorption Process

Negatively and positively charged sites could appear at the brick surface through deprotonation and protonation of -OH groups at proportions that were dependent upon the medium pH. The amphoteric edge hydroxyl groups (denoted here: $\equiv\text{S-OH}$) then accounted for possible chemical equilibria showing partial and specific adsorptions of metallic cation onto modified brick grains as follows:



and/or



Moreover, the interaction of metallic cations with ferrihydrite - coated brick resulted more in inner-sphere complexes [21]. Furthermore, as observed for kaolinite [61] (which also contains $\equiv\text{Si-OH}$ and $\equiv\text{Al-OH}$ groups), the most probable sites for the forming of inner-sphere complexes with Me^{2+} ions were negatively charged edge sites, $\equiv\text{SO}^-$. The Me^{2+} -ions removal from the solution by modified brick resulted in a decrease of solution pH [20,21], however, this increasing of H^+ concentration was largely insufficient to achieve molecular and electric balances and Na^+ ions ought to be taken into account in the process [20,21]. On the other hand, as shown in Fig. 6 the pseudo-second-order kinetics rate, k_2 , was dependent on the hydrolysis characteristics of divalent cations as [61-62]:

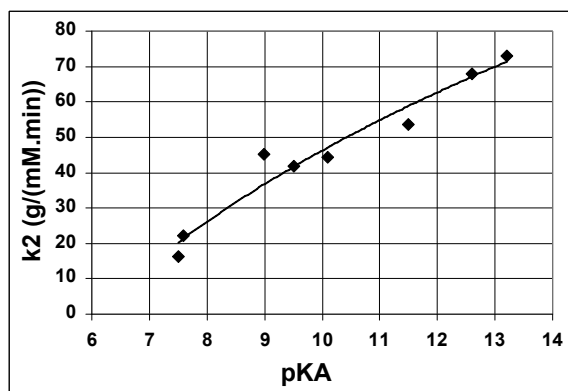
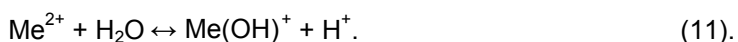
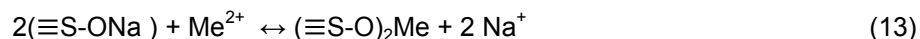
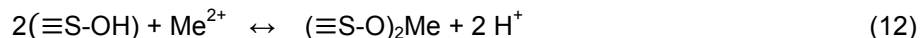


Fig. 6. pK_A-dependence of the pseudo-second order kinetic rate (k₂).
K_A represents the first hydrolysis (acidity) constant of divalent cation [61-63].

All these observations indicated clearly that more the difference between solution pH and pH_{PZC} (the pH value at the point of zero charge, PZC: 3.2) was high and more electrostatic forces increased and facilitated the process in due course. This explained the decrease observed for k_2 values: from 73.0 for Sr^{2+} to 22.2 g/(mM.min) for Pb^{2+} (see Table 3). Deprotonated functional groups (which were previously generated during the preparation / activation of modified brick through Fe(III) precipitation with NaOH), were found to be more beneficial for the adsorption process. Indeed, this chemical treatment led to: (i) few H^+ competing with Me(II) for the adsorption sites of brick; and (ii) more Na^+ ions exchanging predominantly with Me(II) at the water-brick interface.. A general mechanism was then proposed:



The metal binding constants, $K_{(\equiv\text{SOMe})}$ relative to equation 9, which were reported previously for kaolinite [61] (see Table 5), were used in the present work because brick hydroxylation generated hydroxyl groups at the brick-metakaolinite surface with chemical characteristics

similar to those observed at the kaolinite surface. The surface binding constant, $\log[(K_{(=SOMe)})]$, was plotted against the adsorption capacity, Q_e (Fig. 7).

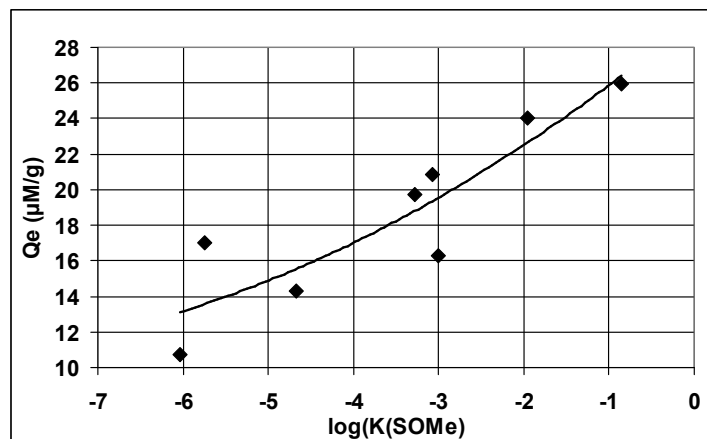


Fig. 7. Correlation of surface complexation constants, $K_{(=SOMe)}$ ^{*}, of eight cations adsorbed onto hydroxyl groups from brick metakaolinite (after its modification) with the amount of adsorbed cation, Q_e , at equilibrium.

(*) Constants for complexation between metals and kaolinite [61].

A relationship was found between this binding constant and Q_e , revealing an implication of hydroxyl groups of metakaolinite in addition to the $-OH$ and/or $-O^-Na^+$ functions of brick ferrihydrite. As a whole, the adsorption affinity of the studied eight elements onto $\equiv S-OH$ sites in modified brick had the following order: $Pb > Cu > Cd \approx Mn \approx Zn > Mg > Ca > Sr$.

To summarize, the magnitude of Q_e was dependent upon complexing interactions between $\equiv S-O^-$ and Me^{2+} , while the kinetic constant was related to electrostatic attractions between charged sites on the brick and ions in water. Therefore, Q_e varied with the stability constant of the generated complex, and k_2 was influenced by H^+ and OH^- (*i.e.*, the pH of the studied suspension) as potential-determining ions by regulating proportions of negative and positive charges at the brick surface.

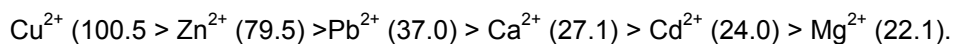
Table 5. First hydrolysis constants, pK_A, of divalent cations and their surface complexation constants, $K_{(=SOMe)}$, when adsorbed onto hydroxyl groups from brick metakaolinite (Q_e represents the amount of adsorbed cations on the equilibrium state)

Cations	Q_e ($\mu\text{mol/g}$)	pK _A ([*])	$\log[(K_{(=SOMe)})]$ ^(§)
Ca ²⁺	17.04	12.6	~-5.75
Cd ²⁺	19.76	10.097	-3.28
Cu ²⁺	24.06	7.497	-1.96
Mg ²⁺	14.33	11.5	~-4.67
Mn ²⁺	20.84	9.5	~-3.07
Pb ²⁺	25.95	7.597	-0.85
Sr ²⁺	10.70	13.2	~-6.03
Zn ²⁺	16.30	8.997	-3.01

(^{*}) First hydrolysis constants from refs [61-63]. ([§]) Constants for complexation between metals and kaolinite [61].

4. CONCLUSION

In this study, a successful ferrihydrite-coated (pre-activated) brick filter was developed for the removal metallic cations from water. This adsorption process was found to be better fitted by Langmuir model. The amount of divalent cations at complete monolayer coverage, Q_{\max} was assessed by Langmuir isotherms and followed a descending sequence (in $\mu\text{mol/g}$):



As for the kinetic aspects of the adsorption reaction, experimental data were described better by the pseudo-second order adsorption kinetic rate model. The corresponding rate constant for this adsorption was found to decrease in the following order (k_2 at $\sim 298^\circ\text{K}$ expressed in $\text{g}/(\text{mM}\cdot\text{min})$): Sr (73.02); Zn (45.06); Fe (44.39); Cd (33.7); Pb (22.23); Cu (16.20). The activation parameters of the kinetics process enabled us to predict how the adsorption of divalent cations varied with temperature changes: (i) the Gibbs free energy of activation and the activation enthalpy revealed an endothermic performance for the adsorption of Me^{2+} ions onto modified brick; and (ii) the activation entropy reflected the decrease of randomness at the solid-solute interface mainly as a consequence of electrostatic attraction followed by an intermediate hydroxyl complexation in the ferrihydrite phase: such a combination was thought to form with time inner-sphere complexes on negatively charged sites of the brick.

The differences observed in kinetic rate constants towards the sorbent surface were related mostly to the acidic (hydrolysis) properties of these divalent cations in water ($\text{p}K_A$) and the pH-dependence of the brick-surface charges. This suggested that H^+ and OH^- are potential -determining ions in the electrokinetic behavior of ions adsorption onto solids by generating electrostatic forces at the brick-water interface, as already suggested by Wiese and his coworkers [64]. Moreover, the amount of adsorbed cations at the equilibrium state (Q_e) – which was evaluated from kinetic studies— followed the decreasing order: $\text{Pb} > \text{Cu} \sim \text{Cd} > \text{Zn} > \text{Mg}$. This order resulted in the extent of complexation between active brick sites and cations in aqueous solution. This hypothesis was sustained by a relationship between Q_e and the surface binding constant, $K_{(\text{SOMe})}$ in kaolinite.

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COMPETING INTERESTS

Authors have declared that no competing interests exist.

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